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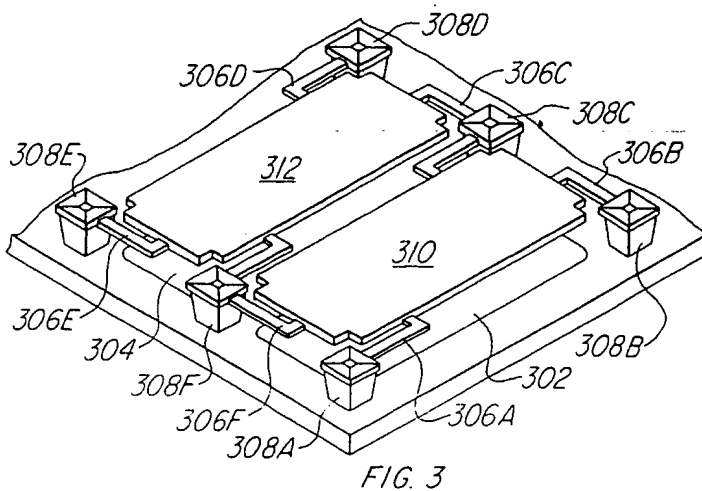
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(54) Improvements in or relating to light modulation.

(57) It is possible to describe how to control the amplitude and phase modulation of light independently and simultaneously do so by dividing a picture element into smaller modulating elements, providing independent addressing for each element, setting the necessary angle for each element and then resolving them into the picture element. The invention also shows one embodiment of the invention.



The present invention relates to methods of light modulation and spatial light modulators, including phase modulators and full complex light modulators.

Spatial light modulators (SLMs) are devices used to control the distribution of light in an optical system. Spatial light modulators are divided into one- or two-dimensional arrays of modulation elements called pixels, or picture elements, that represent the smallest addressable unit within the device. The SLM pixel is used to modify either the amplitude or the phase of the light distribution within the optical system.

In practice, the light modulation characteristics of most prior art SLMs are coupled combinations of amplitude and phase changes. The modulation characteristic of a pixel is controlled by a single applied signal, either an electrical voltage, current or incident optical intensity level, so the amplitude and phase characteristics of the pixel can not be independently set.

There are numerous applications, especially in optical information processing, in which controlling amplitude and phase independently is essential. Phase modulation is essential since most of the signal information is contained in the phase terms. The additional control of amplitude provides means for rejecting noise in the filter plane for improved system performance.

Four major types of modulators are presently being used for phase modulation; liquid crystal, photorefractive, magneto-optic, and deformable mirror. All have coupled phase and amplitude modulation characteristics.

Liquid crystals allow for phase and amplitude modulation, but phase modulation has extremely narrow ranges for the electric fields applied for uniform realignment, making it hard to control. Amplitude modulation is also difficult since the nonuniform realignment causing the amplitude modulation also contributes to phase modulation, resulting in a phase-amplitude coupled modulation.

Photorefractive modulators work for phase-only modulation only at extremely high voltages. Birefringence caused in nonuniform alignment produces amplitude modulation. But since photorefractive, like liquid crystal, modulates by a change in the refractive index, phase modulation accompanies amplitude modulation.

Magneto-optic modulators produce a binary change in the polarization of light, but are hard to control in operation. Kast, et al., in their article in *Applied Optics*, 15 March 1989, describe a method for ternary operation of magneto-optic modulators, but it has a very limited range of amplitude- or phase-only modulations, none of which are independently controlled.

Present deformable mirror devices could be effective if the resolution of the optical system was fine enough to resolve the mirror element separate from the background. But, the normal setting for resolution of optical systems is the Nyquist frequency, causing the mirror to be mixed with the background. Amplitude modulation results from the interference between the two distributions.

Two other methods of phase-only modulation have been used. The first method was introduced by Brown and Lohmann in *Applied Optics*, 1966. Their technique, detour phase, requires very tight system alignment and limited field-of-view for the phase encoding approximations to be valid. The second was introduced by Hansche, et al., in their article in *Applied Optics*, 15 November, 1989. Their approach allows for different amplitudes to be produced, but requires a lowered resolution in the optical system.

According to the present invention in a first aspect thereof, a method for modulation of light comprises the following steps:

- a) dividing a picture element into a number of modulating elements;
  - b) providing addressing circuitry for each said modulating element;
  - c) selecting the desired phase angle and amplitude of modulation;
  - d) determining appropriate displacement angles of said modulating elements to achieve said phase angle and amplitude;
  - e) addressing said modulating elements to achieve desired angle; and
  - f) resolving said modulation elements as said picture element preferably said addressing of said modulating elements consists of applying a predetermined voltage to an electrode located directly under said modulating element. The said modulation may be amplitude modulation or full complex modulation.
- According to the present invention in a second output thereof a spatial light modulator, comprises:
- a) a plurality of picture elements formed in a layered structure, each pixel being divided into a number of modulating elements;
  - b) said layered structure including a substrate, a spacer layer on said substrate, a reflecting layer on said spacer, and electrical addressing circuitry;
  - c) each of said modulating elements being an electrostatically deflectable element formed in said reflecting layer, and said spacer defining a well located between said deflectable element and a plurality of activation electrodes arranged to affect said electrostatic deflection; and
  - d) electrical addressing circuitry such that each of said modulating elements are independently address-

sable.

Preferably

said modulator is divided into two halves. Advantageously said addressing circuitry includes a plurality of activation electrodes; one electrode corresponding to each modulating element.

As part of this application an exemplary method and apparatus for full complex light modulation is described. Full complex light modulation allows the modulation of a signal with independent control of phase and amplitude.

The method described uses a standard picture element. The picture element is then divided into a number of smaller modulating elements. Each modulating element is provided with its own circuitry for addressing. The net phase angle,  $\Phi$ , and the desired resultant amplitude, A, must be selected. Through a series of calculations using A and  $\Phi$ , a number of angles can be found. These angles,  $\theta_1$ ,  $\theta_2$ , etc. are for the individual modulating elements.

The addressing circuitry for the individual modulating elements is then activated in such a way as to cause the modulation at the angle  $\theta_x$ . The light signal is then directed to the picture element and its individual modulating elements. The final step in the process occurs when the optical system scans the modulating elements and resolves them as if they were the whole picture element.

The preferred embodiment shown uses a deformable mirror device (DMD) as the picture element. A flexure beam DMD is cut into a number, for example two, of smaller flexure beam DMDs. The addressing circuitry in this case is electrodes, which are located underneath each half of the picture element. The angles,  $\theta_1$ , and  $\theta_2$ , are caused when a voltage is applied to the electrodes. The value of the voltage applied determines the value of the angle. The preferred embodiment shows only two modulating elements but it is possible to use this method for more than two angles.

For a more complete understanding of the present invention, and the advantages thereof, reference is now made to the following description, given by way of example only, taken in conjunction with the accompanying drawings, in which:

FIGURE 1 shows the flow chart of the process for full complex light modulation;

FIGURE 2 shows a perspective view of a prior art flexure beam deformable mirror device (DMD);

FIGURE 3 shows a perspective view of a divided flexure beam DMD according to the present invention;

FIGURE 4 is a top view of the divided DMD; and

FIGURE 5 shows one example of a DMD divided into more than two modulating element.

The flowchart for the process of full complex light modulation is illustrated in FIGURE 1. In step 102, the pixel is divided into however many modulating elements are desired within a pixel. Step 104 provides for addressing circuitry for each modulating element within the pixel, so each is individually addressable. Step 106 is the point at which the type of modulation must be selected.

If amplitude and phase modulation is desired, it is possible to perform both simultaneously. The process continues in this case to step 108.

In this step, the desired amplitude, A, and net phase angle,  $\Phi$ , must be selected. Once those two variables are set, the angles for the individual modulating elements must be determined, in step 110. The complete analytical description of the optical distribution transmitted by, or reflected by, the full complex pixel is given by equation (1):

$$p(x, y) = [b + me^{j\theta_1}] \text{rect} \left[ \frac{x}{w_x}, \frac{y - \frac{W}{4}}{w_y} \right] + [b + me^{j\theta_2}] \text{rect} \left[ \frac{x}{w_x}, \frac{y + \frac{W}{4}}{w_y} \right] \quad (1)$$

where  $w_x$  and  $w_y$  are the widths of the modulating elements in the horizontal and vertical direction, W is the width of the entire square pixel region, and  $\theta_1$  and  $\theta_2$  are the phase setting of the individual modulators.

With the optical system resolution set to pass the 0,0 diffraction order Nyquist passband for array elements of width W, the net response of this pixel is determined by equation (2):

$$r(x, y) = p(x, y) * \text{sinc} \left[ \frac{x}{W}, \frac{y}{W} \right] \quad (2);$$

where the asterisk represents a two-dimensional convolution. This equation represents a complicated spatial

distribution that cannot be simplified. However, the distribution is essentially a two-dimensional sinc function of width slightly greater than  $2W$  and a peak complex amplitude given by equation (3):

$$Ae^{j\Phi} = b + me^{j\theta_1} + b + me^{j\theta_2} \quad (3),$$

where  $A$  and  $\Phi$  are the amplitude and phase values of the net pixel response resulting from the coherent mixing of the two phase modulator responses.

At any specific net phase value  $\Phi$ , there is a maximum possible net amplitude,  $A$ . The maximum value occurs when the two modulator phase settings are equal,

$\theta_1 = \theta_2 = \theta$  giving:

$$A_{\max} = 2\sqrt{b^2 + m^2 + 2mb\cos\theta} \quad (4).$$

However, to specify this maximum value, it is first necessary to determine the proper phase setting  $\theta$  to find the net phase angle  $\Phi$ . The geometrical analysis to make this determination is quite involved resulting in the following relationship

$$\theta = \cos^{-1} \left[ \frac{-mb[1 - \cos^2\Phi] \pm \sqrt{[m^4 + m^2b^2]\cos^2\Phi + m^2b^2\cos^4\Phi}}{m^2} \right] \quad (5).$$

This expression gives two values for the phase angle  $\theta$  corresponding to angles in the upper or lower half plane. The proper choice is the angle that lies in the same half plane as  $\Phi$ . The geometrical analysis again gives the prescription for specifying the phase settings,  $\theta_1$  and  $\theta_2$ , to achieve the desired net amplitude and phase values,  $A$  and  $\Phi$ . These phase settings are

$$\theta_1 = \phi_0 + \Delta\phi \quad (6),$$

$$\theta_2 = \phi_0 - \Delta\phi \quad (7);$$

where

$$\phi_0 = \tan^{-1} \left[ \frac{A \sin\Phi}{A \cos\Phi - 2b} \right] \quad (8),$$

and

$$\Delta\phi = \cos^{-1} \left[ \frac{\sqrt{A \cos\Phi - 2b^2 + A \sin^2\Phi}}{2m} \right] \quad (9).$$

These formulas are the specific ones for two halves of a given pixel. It is possible to use this method of analysis for more than two angles.

Step 112 requires the application of the voltages in order to deflect the appropriate modulating elements to achieve the phase angles calculated in step 110. The voltage to achieve a certain angle can be found by the following relationship:

$$V = \sqrt{\frac{K\lambda\theta[4\pi d_o - \lambda\theta]^2}{64\pi^3\epsilon_o A}} \quad (10),$$

where  $V$  is the applied voltage,  $K$  is the spring constant of the DMD hinge,  $\theta$  is the angle of deflection,  $d_0$  is the distance of the DMD from the electrode before deflection,  $\lambda$  is the wavelength of the incident light, and  $\epsilon_0$  is the electrical permittivity of free space.

Step 114 is the part of the process that an actual optical signal is applied to the set elements by the system. Step 116 allows all of the independently addressed modulating elements to be integrated into one pixel. In this context, integration is the actual scanning done by the optical system, where the individual elements are grouped back into the original pixel. That is, the modulating elements, taken together are scanned by the optical system as though they were a single pixel.

If amplitude-only modulation is desired, the process steps to 118. The modulated amplitude,  $A$ , is selected. Using equations 6, 7, 8, and 9, it is possible to again solve for the individual angles,  $\theta_1$  and  $\theta_2$ , in step 120. The relationship for the voltage set out in equation 10 is again used to determine the amount of applied voltage necessary for the proper deflection and applied in step 122. Step 124 again requires the direction of light, and step 126 is the integration of the modulation elements into the original pixel.

With the embodiment described phase-only modulation is also possible. The process moves to step 128. The angle selected for phase modulation is the angle for the individual modulating elements. Using equation 10 to determine the proper voltage, all individual modulating elements are set to that angle in step 130. After directing the light onto the modulating elements in step 132, each individual piece of the original pixel is treated as its own pixel. For example, if there existed an original array of  $N \times N$  pixels, and each pixel was divided into two modulating elements, the system would scan an array of  $N \times 2N$  pixels at step 134.

FIGURE 2 shows a prior art configuration of a flexure beam DMD. An addressing electrode 206 is built onto a substrate 202. A mirror element 210 is built onto a spacer covering the layer containing 206. The spacer layer is then etched away. This leaves a layer of support posts 204A, 204B, 204C, and 204D, with an gap between the mirror element 210 and the electrode 206. When a pre-determined voltage is applied to electrode 206, mirror element 210 is electrostatically attracted to it. The flexure hinges 208A, 208B, 208C, and 208D, allow the mirror to deflect downwards. Because all four corners are supported, the mirror deflects with a piston-like movement.

FIGURE 3 illustrates a divided DMD with two individual modulating elements. If a voltage is applied to address electrodes 302, then mirror 310 will deflect downwards flexing on hinges 306A, 306B, 306C, and 306F. Mirror 312 will not deflect unless a voltage is applied to address electrode 310, allowing independent operation of the two mirror elements. As in FIGURE 2, the flexure hinges 306A, 306B, 306C, 306D, 306E, and 306F, are supported by support posts 308A, 308B, 308C, 308D, 308E, and 308F, creating a gap between the mirror elements 310 and 312 and electrodes 302 and 304, respectively.

The top view of the divided pixel is shown in FIGURE 4. The variables used in the above equations are shown.  $W_x$  is along the horizontal axis, as indicated by the double-headed arrow 401, the distance from support post 402A to support post 402B.  $W_y$  is along the vertical axis, indicated by the double-headed arrow 403, either from support post 402B to 402C, or from support post 402C to support post 402D. In this case, the pixel was divided horizontally into two parts, so there are two  $w_y$  to one  $w_x$ . Mirror elements 404 and 406 are individually addressable underneath the mirror surface, as seen in the perspective drawing of FIGURE 3. The preferred embodiment has  $w_x$  equal to about  $50 \mu\text{m}$ .  $W_y$  would be about half of that, about  $25 \mu\text{m}$ . Since  $w_x$  is the same as the side length  $W$ , the active area of an undivided pixel in this case would be  $2500 \mu\text{m}^2$ . Due to loss of area from the gap between the two mirrors, support posts and hinges, the active area is actually about  $2125 \mu\text{m}^2$ . An advantage of this embodiment is that the divided pixel still has eighty-five percent of its original active area.

FIGURE 5 shows an example of one possible other division of a pixel. The pixel is divided into two individual elements, which are in turn divided into two pieces. The mirror 502 has addressing electrode 510, and each other modulating element has a corresponding element, making all of them individually addressable.

A feature of the present invention is that it may be applied to existing systems by replacing picture elements with divided picture elements in accordance with the present invention, for example prior art DMDs with divided DMDs. The optical arrangement of such existing system will inherently resolve such a divided pixel as a single picture attempt. Thus full complex modulation capability may be added to the existing system.

#### Claims

1. A method for modulation of light comprising the following steps:
  - a) dividing a picture element into a number of modulating elements;

- b) providing addressing circuitry for each said modulating element;
- c) selecting the desired phase angle and amplitude of modulation;
- d) determining appropriate displacement angles of said modulating elements to achieve said phase angle and amplitude;
- 5 e) addressing said modulating elements to achieve desired angle; and
- f) resolving said modulation elements as said picture element.

2. The method of claim 1, wherein:

- a) said addressing of said modulating elements consists of applying a predetermined voltage to an electrode; located directly under said modulating element.

3. A method as claimed in claim 1 or claim 2 and wherein said modulation is amplitude modulation.

4. A method as claimed in claim 1 or claim 2 and wherein said modulation is full complex modulation.

5. A spatial light modulator, comprising:

- a) a plurality of picture elements formed in a layered structure, each pixel being divided into a number of modulating elements;
- b) said layered structure including a substrate, a spacer layer on said substrate, a reflecting layer on said spacer, and electrical addressing circuitry;
- c) each of said modulating elements being an electrostatically deflectable element formed in said reflecting layer, and said spacer defining a well located between said deflectable element and a plurality of activation electrodes arranged to affect said electrostatic deflection; and
- d) electrical addressing circuitry such that each of said modulating elements are independently addressable.

6. The modulator of claim 5, wherein:

- a) said modulator is divided into two halves.

7. The modulator of claim 1, 5 or claim 6, wherein:

- a) said addressing circuitry includes a plurality of activation electrodes; one electrode corresponding to each modulating element.

8. A picture element modulator divided into a number of individual modulating elements.

9. A deformable mirror device divided into a number of individual modulating elements.



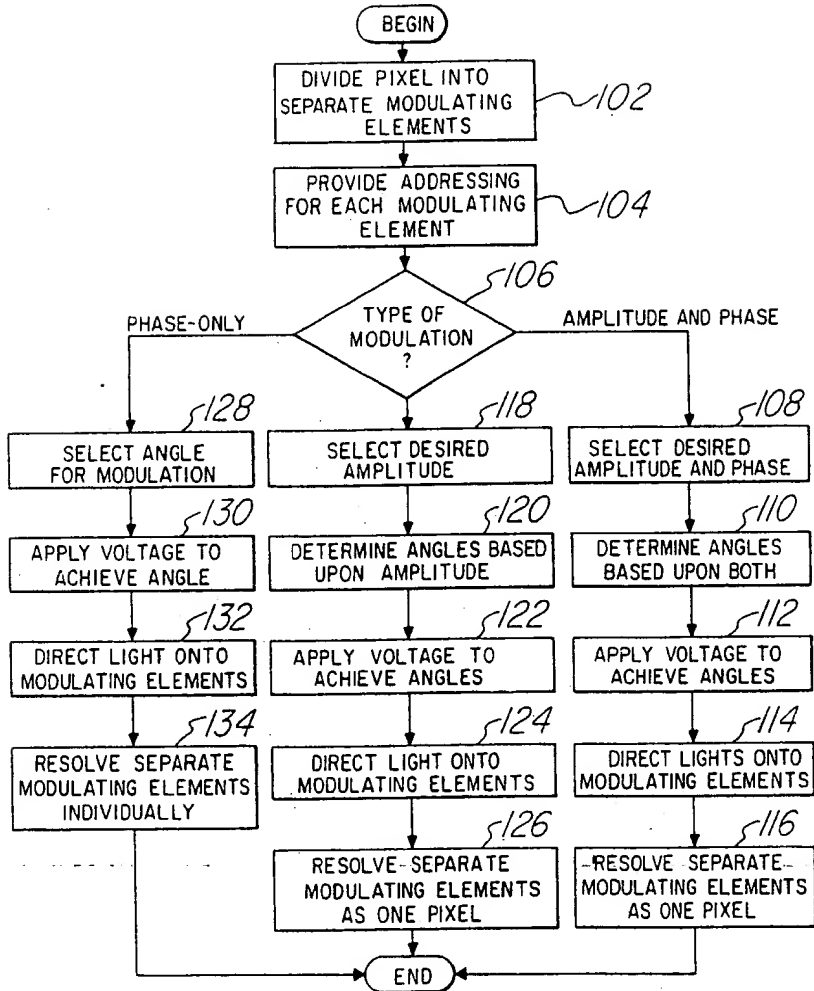


FIG. 1

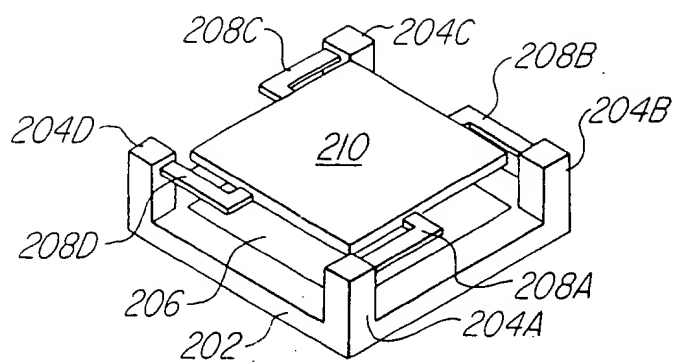


FIG. 2

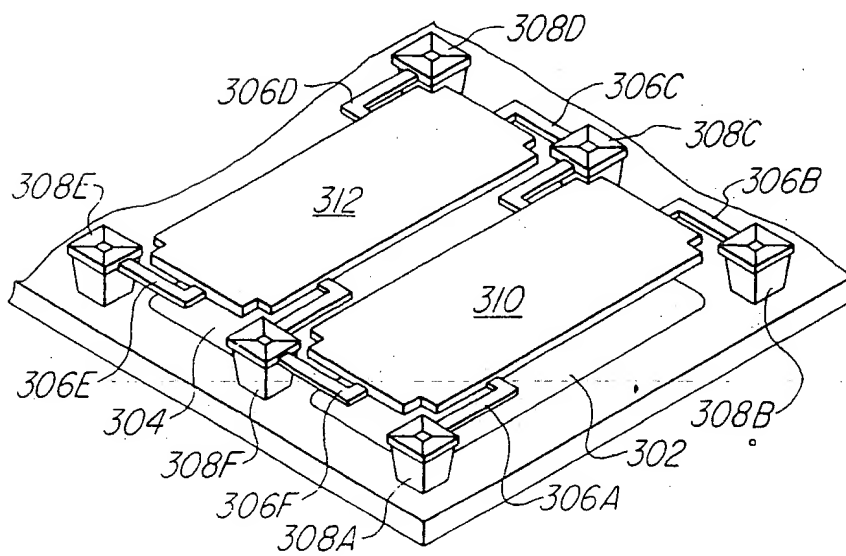


FIG. 3

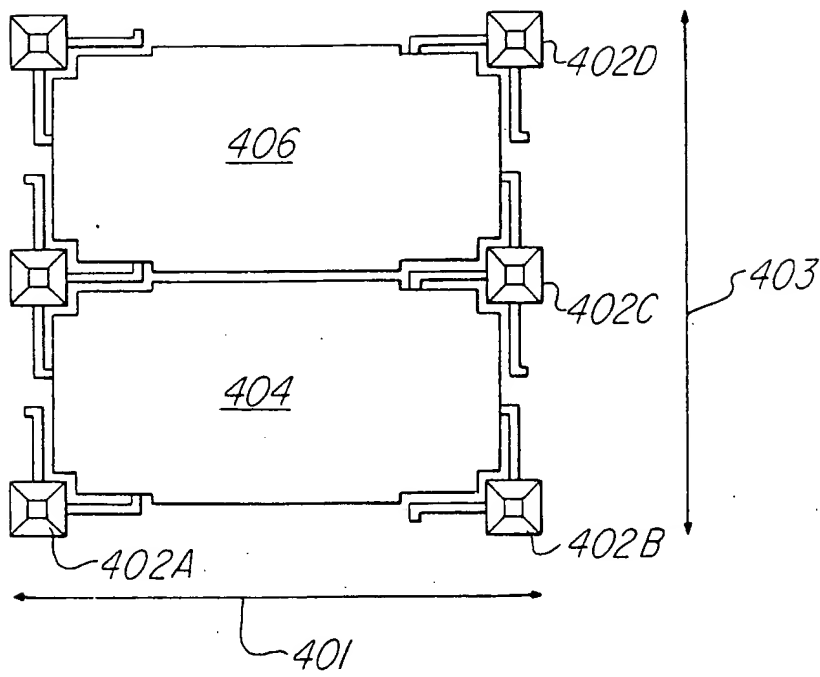
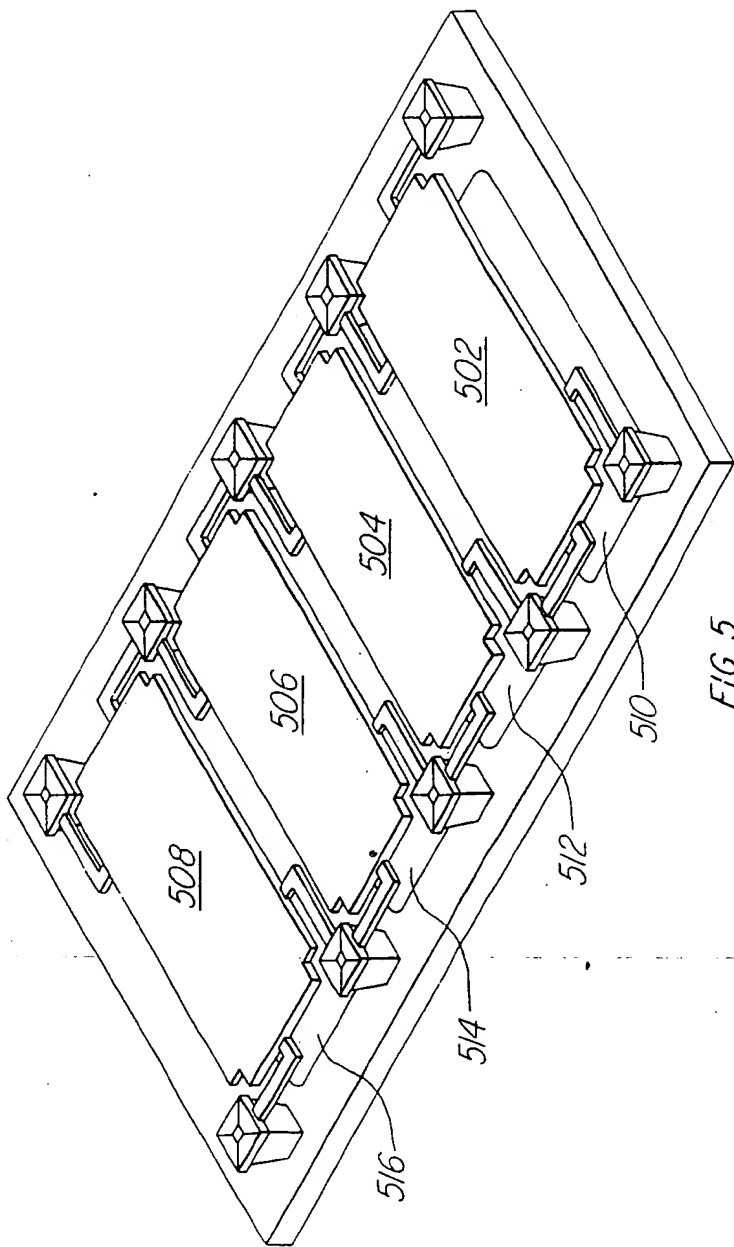


FIG. 4





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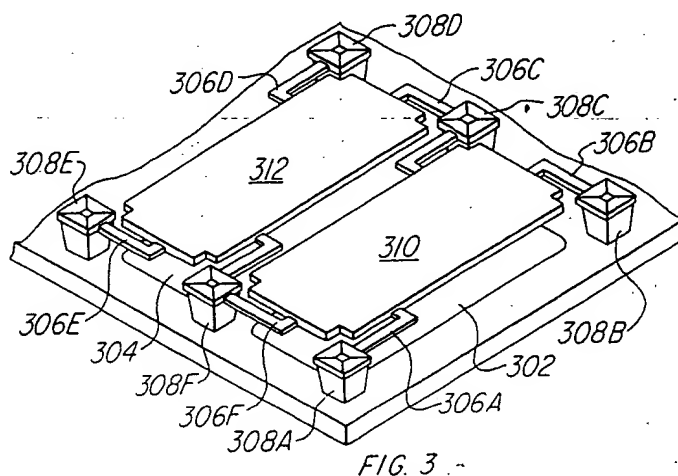


FIG. 3



European Patent  
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# EUROPEAN SEARCH REPORT

Application Number

EP 91 11 4435

| DOCUMENTS CONSIDERED TO BE RELEVANT   |  |   |   |
|---|--|---|---|
| Category  | Citation of document with indication, where appropriate, of relevant passages  | Relevant to claim                                 | CLASSIFICATION OF THE APPLICATION (Int. Cl.5)             |
| Y<br>A<br>X   | US-A-4 954 789 (SAMPSELL)<br><br>* column 5, line 60 - column 8, line 11; figures 1-3 *<br>---   | 1-4<br>5-7<br>8,9                                 | G02B26/08<br>G09F9/37                                     |
| Y<br><br>A<br>X   | OPTICAL ENGINEERING<br>vol. 22, no. 6, December 1983,<br>pages 675 - 681;<br>D.R. PAPE & L.J. HORNBECK: 'Characteristics of the deformable mirror device for optical information processing'<br><br>* abstract *<br>* page 676, right column, line 8 - page 679, left column, line 5; figures 1,2 *<br>--- | 1-4<br><br>5-8<br>9                               |   |
| A<br>X  | EP-A-0 332 953 (TEXAS INSTRUMENTS)<br><br>* page 2, line 16 - line 22; claim 6 *<br>* page 7, line 23 - page 8, line 22; figures 1,2 *<br>---  | 1-3<br>5,7-9                                      | TECHNICAL FIELDS SEARCHED (Int. Cl.5)<br><br>G02B<br>G09F |
| The present search report has been drawn up for all claims  |  |   |   |
| Place of search<br>THE HAGUE  |  | Date of completion of the search<br>16 MARCH 1992 | Examiner<br>LIPP G.                                       |
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